

High order explicit Runge-Kutta pairs for ephemerides of the Solar System and the Moon

PHILIP W. SHARP †

sharp@math.auckland.ac.nz

*Department of Mathematics, University of Auckland, Private Bag 92019,
Auckland, NEW ZEALAND.*

Abstract. Numerically integrated ephemerides of the Solar System and the Moon require very accurate integrations of systems of second order ordinary differential equations. We present a new family of 8-9 explicit Runge-Kutta pairs and assess the performance of two new 8-9 pairs on the equations used to create the ephemeris DE102. Part of this work is the introduction of these equations as a test problem for integrators of initial value ordinary differential equations.

1. Introduction

An ephemeris of the planets and the Moon consists of tabular information from which accurate positions and velocities of the celestial bodies can be calculated for any value of astronomical time on a prescribed range. Modern ephemerides typically contain accurate values of the position and velocity at equally spaced astronomical times, and the coefficients of Chebyshev polynomials for interpolation between the values.

The information in an ephemeris can be obtained by numerically integrating a system of ordinary differential equations that model all significant gravitational attractions between the bodies. To take full advantage of the accuracy of modern astronomical observations and to distinguish between competing analytical theories for the motion of the bodies, the global error in the integrations must be very small. Another characteristic of the integrations is that they often span a large interval of astronomical time, necessitating many integration steps.

The accumulated round-off error in an integration will in general grow as an integration proceeds. If the integration is done in double precision arithmetic, the accumulated round-off error may be far larger than the required accuracy. This difficulty can be overcome by using 80-bit arithmetic or even quadruple precision.

The ordinary differential equations for ephemerides are non-stiff and hence explicit Runge-Kutta (ERK) pairs are suitable methods for performing the integrations. Pairs consist of formulae of orders p and q , where $q < p$ and is typically $p - 1$. The computational effort required to advance a step with a pair can be measured by the number of derivative evaluations, known as stages, performed on the step. For conciseness, we refer to a pair of s stages as an s -stage $q - p$ pair.

† This work was supported by the University of Auckland Research Committee.

Of the many ERK pairs available, the 13-stage 7-8 pair of Prince and Dormand [6] has proven to be as efficient as any other on many problems when using double precision arithmetic, except possibly for low accuracy requirements.

In particular, the pair is noticeably more efficient than 8-9 pairs. We investigate whether this result holds for numerically integrated ephemerides. In section two, we summarise the derivation of two families of 8-9 pairs, one of which is a new family, and present a near optimal pair from each family. In section three, we compare the performance of the two new pairs and the 7-8 pair of Prince and Dormand on the model equations of DE102. We end in section four with a discussion of our work.

2. Order nine pairs

2.1. Definitions

Consider the initial value problem

$$y' = f(x, y), \quad y(x_0) = y_0, \quad (1)$$

where $' \equiv d/dx$, $f : \mathbb{R} \times \mathbb{R}^n \rightarrow \mathbb{R}^n$ and the solution $y(x)$ is sufficiently differentiable.

The 8-9 ERK pairs we investigate have s -stages and generate an order nine approximation y_i and an order eight approximation \hat{y}_i to $y(x_i)$, $i = 1, 2, \dots$, according to

$$y_i = y_{i-1} + h \sum_{j=1}^s b_j f_j, \quad (2)$$

$$\hat{y}_i = y_{i-1} + h \sum_{j=1}^s \hat{b}_j f_j, \quad (3)$$

where $h = x_i - x_{i-1}$ and

$$f_j = f(x_{i-1} + hc_j, y_{i-1} + h \sum_{k=1}^{j-1} a_{jk} f_k), \quad j = 1, \dots, s, \quad (c_1 = 0).$$

We refer to c_j , $j = 1, \dots, s$, as the abscissae, a_{ij} , $j = 1, \dots, i-1$, $i = 2, \dots, s$, as the interior weights, b_j , \hat{b}_j , $j = 1, \dots, s$, as the exterior weights, and to the abscissae, the interior weights and the exterior weights collectively as the coefficients of the pair. To ensure the one step nature of the pairs, we restrict the abscissae to the interval $[0, 1]$.

When the coefficients of the pair are chosen so that y_i and \hat{y}_i are order nine and eight respectively, some coefficients are available as free parameters, leading to a family of pairs and not a unique pair. Individual pairs from this family are obtained by assigning values to the free parameters. Since we are interested in doing very accurate integrations, we have chosen the values so that the local error introduced on a single step is close to the minimum possible when using small stepsizes.

This error for the step from x_{i-1} to x_i can be written as (for, example [3], page 151)

$$h^{10} \sum_{t \in T_{10}} e_{10}(t) D_{10}(t) + O(h^{11}),$$

where T_{10} is the set of rooted trees of order ten, $e_{10}(t)$ is the principal error coefficient for tree t , and $D_{10}(t)$ is the elementary differential for t . The elementary differential is formed from the partial derivatives of f with respect to x and y and evaluated at (x_{i-1}, y_{i-1}) .

The principal error coefficient for tree t can be written as

$$e_{10}(t) = \frac{\alpha(t)}{10!} (\gamma(t) \sum_{k=1}^s b_k \phi_k(t) - 1),$$

where $\alpha(t)$ and $\gamma(t)$ are positive integers, and $\phi_k(t)$ is a function of the interior weights and abscissae.

Numerical experiments have shown (see, for example [6]) that decreasing the size of the principal error coefficients will in general improve the efficiency of the method. Hence, we choose the free parameters so that the error coefficients are close to their minimum value.

We use two measures of the size of the principal error coefficients

$$E_{10}^2 = \left[\sum_{t \in T_{10}} e_{10}^2(t) \right]^{1/2}, \quad E_{10}^\infty = \max_{t \in T_{10}} \{|e_{10}(t)|\}. \tag{4}$$

2.2. Sixteen stages

Verner [9] derived a family of 16-stage 8-9 pairs with $c_2, c_5, c_9, c_{10}, c_{11}, c_{13}, c_{14}$ and $a_{11,6}$ as free parameters (To simplify what follows, we have interchanged the coefficients for the fourteen and sixteenth stages, this can be done without changing the properties of the pairs.) The order nine formula in the pairs uses the first fifteen stages and the order eight formula uses all sixteen stages. The coefficients $b_j, \hat{b}_j, j = 2, \dots, 7, b_{16}, \hat{b}_{14}$ and \hat{b}_{15} are identically zero.

Verner presented the coefficients of a pair from this family which had $c_2 = 1/12, c_5 = (2 + 2\sqrt{6})/15, c_9 = 1/2, c_{10} = 1/3, c_{11} = 1/4, c_{13} = 5/6, c_{14} = 1/6$ and $a_{11,6} = 0$. The pair has $E_{10}^2 = 6.1 \times 10^{-5}$ and $E_{10}^\infty = 3.1 \times 10^{-5}$, and has been used when comparing the numerical performance of 8-9 pairs with pairs of other orders. However, the pair was intended as an illustration of the derivation and not as an optimal or near optimal pair.

To assess in a problem-independent way if the 8-9 family of Verner contains more efficient pairs, and if so, how much more efficient, we performed a minimisation of E_{10}^2 over the free parameters, subject to the constraint that the coefficients of the pair be no larger than M in magnitude. This constraint is commonly used when

selecting a pair from a family and is intended to prevent the selection of a pair with poor round-off error properties. Although no one value of M is used, it is often 20 or 30 and we chose 30.

We performed the minimisation using an interactive grid search and obtained a minimum value for E_{10}^2 of 7.5×10^{-7} when working with a grid size of 0.001. The pair we obtained had $c_2 = 0.020$, $c_5 = 0.311$, $c_9 = 0.312$, $c_{10} = 0.105$, $c_{11} = 0.587$, $c_{13} = 0.879$, $c_{14} = 0.916$ and $a_{11,10} = -0.150$ (as a matter of preference we have used $a_{11,10}$ in place of $a_{11,6}$ as a free parameter). The algorithms in [9] can be used to find the remaining coefficients. The pair has $E_{10}^\infty = 2.8 \times 10^{-7}$.

A slightly smaller value of E_{10}^2 is possible if a smaller grid size is used, but since the number of derivative evaluations varies approximately as the ninth root of E_{10}^2 , the gain in efficiency is small. A significantly smaller value of E_{10}^2 , approximately twice as small, is possible if the abscissae are not constrained to the interval $[0, 1]$, but this choice means the pair is no longer a one step method.

An estimate of the efficiency of the new pair relative to that of Verner can be calculated by using E_{10}^2 for the two pairs. To do this, we assume the global error for a fixed t and stepsize is proportional to E_{10}^2 . The relative efficiency is then estimated as

$$\left[\frac{3.1 \times 10^{-5}}{7.5 \times 10^{-7}} \right]^{1/9} = 1.63 \dots$$

This suggests the new pair will be approximately 63 percent more efficient than the pair of Verner at small stepsizes, raising the possibility of it being competitive with pairs of other orders.

2.3. Seventeen stages

The work of Sharp and Smart [7] for 4-5 and 5-6 ERK pairs shows a gain in efficiency is possible if an extra stage is used to form the pair. The extra stage means more free parameters are available, permitting a smaller value of E_{10}^2 , but this is at the expense of increasing by one the number of function evaluations required to take a step.

To investigate if a gain in efficiency was possible for 8-9 pairs, we derived a family of 17-stage 8-9 pairs. The family has six more free parameters (three abscissae, three interior weights) than the 16-stage 8-9 pairs.

We impose, as is commonly done for high order ERK pairs (see, for example [9], [11]), the following conditions on the coefficients of the pair

$$\frac{c_i^{k+1}}{k+1} = \sum_{j=1}^{i-1} a_{ij} c_j^k, \quad k = 0, \dots, \xi_i - 1, \quad i = 1, \dots, s, \quad (5)$$

$$a_{ij} = 0, \quad \text{if } \xi_i > \xi_j + 1, \quad j = 1, \dots, i-1, \quad i = 1, \dots, s. \quad (6)$$

The imposition of these conditions reduces the number of independent order conditions and their nonlinearity in the interior weights.

The conditions can be represented by the stage-order vector $\xi = [\xi_1, \xi_2, \dots, \xi_{s-1}]^T$. The 16-stage pairs have $\xi = [5, 1, 2, 3, 3, 3, 4, 4, 5, 5, 5, 5, 5, 5, 5]^T$; to obtain ξ for the 17-stage pairs, one positive integer less than five must be inserted. We examined three choices and found that inserting a 4 after the second 4 to give

$$\xi = [5, 1, 2, 3, 3, 4, 4, 4, 5, 5, 5, 5, 5, 5, 5]^T$$

led to the largest number of free parameters.

With ξ specified, the derivation is similar to that for the 16-stage pairs, the main difference being fewer constraints on the abscissae for the first nine stages. We took $c_2, c_5, c_6, c_7, c_9, c_{10}, c_{11}, c_{12}, c_{14}, c_{15}, a_{8,7}, a_{11,10}, a_{12,10}, a_{12,11}$ as free parameters; other choices are possible, but the number of free parameters remains the same. The abscissae c_3, c_4, c_8, c_{16} and c_{17} are constrained as

$$\begin{aligned} c_3 &= \frac{2}{3}c_4, & c_4 &= \frac{3c_6 - 4c_5}{4c_6 - 6c_5}c_6, \\ c_8 &= c_9 \frac{20c_6c_7 - 15c_6c_9 - 15c_7c_9 + 12c_9^2}{5(3c_9^2 - 4c_6c_9 + 6c_6c_7 - 4c_7c_9)}, & c_{16} &= c_{17} = 1. \end{aligned} \tag{7}$$

The expression for c_{13} is the same as for c_{12} in the 16-stage pairs except c_8, c_9, c_{10} and c_{11} are replaced by c_9, c_{10}, c_{11} and c_{12} respectively.

We performed a minimisation of E_{10}^2 for the new family using an interactive grid search and steepest descent (a grid search by itself was impracticable because of the large number of free parameters) and obtained a pair with $E_{10}^2 = 1.0 \times 10^{-7}$ and $E_{10}^\infty = 3.6 \times 10^{-8}$. The value of the free parameters to four decimal places are $c_2 = 0.0757, c_5 = 0.3617, c_6 = 0.4139, c_7 = 0.1074, c_9 = 0.7607, c_{10} = 0.6068, c_{11} = 0.1531, c_{12} = 0.8333, c_{14} = 0.9733, c_{15} = 0.9888, a_{8,7} = -0.0001, a_{11,10} = -0.0078, a_{12,10} = 0.0067$ and $a_{12,11} = -0.0026$. Equations (7) together with ξ given above and the algorithms in [9] can be used to find the remaining coefficients.

In a similar way to that for the two 16-stage pairs, E_{10}^2 can be used to estimate the relative efficiency of the new 16-stage and 17-stage pairs. We get

$$\left[\frac{7.5 \times 10^{-7}}{1.0 \times 10^{-7}} \right]^{1/9} \frac{16}{17} = 1.18 \dots,$$

where the factor (16/17) is the ratio of the number stages. Hence we expect the new 17-stage pair to be about 18 percent more efficient than the new 16-stage pair for small stepsizes.

2.4. Generalised

The families of 8-9 pairs described in the previous sub-section are readily generalised to include either one or two extra free parameters.

One generalisation is to replace $\hat{b}_j, j = 1, \dots, s$ by the convex linear combination $\alpha b_j + (1 - \alpha)\hat{b}_j$. This substitution is equivalent to making one of the previously

identically zero \hat{b} a free parameter. The local error estimate for the pair is changed, but since b_j , $j = 1, \dots, s - 1$ remain the same, the principal error coefficients of the order nine formulae and hence E_{10}^2 (and E_{10}^∞) are unchanged.

The second generalisation is based on a transformation obtained by Verner [10] for two families of 8-stage 5-6 ERK pairs. Verner showed the family of Prince and Dormand [6] which has c_2, c_3, c_5, c_6, b_8 and \hat{b}_7 as free parameters can be obtained from the family of Verner [9] which has c_2, c_3, c_5 and c_6 as free parameters using a simple transformation on the last two rows of interior weights.

This transformation generalises (Verner, private communication) to other families of pairs, including the 8-9 pairs in this paper. This means b_{16} and \hat{b}_{15} , previously zero in the 16-stage 8-9 pairs, and b_{17} and \hat{b}_{16} , previously zero in the 17-stage 8-9 pairs, can be free parameters.

The introduction of these two free parameters changes the local error estimate and the principal error coefficients of the order nine formula. However, as is the case for the 5-6 pairs in [9], the change in E_{10}^2 and E_{10}^∞ is small for near optimal pairs.

3. DE102

Newhall, Standish and Williams [5] presented DE102, an ephemeris of the Solar System and the Moon, obtained by integrating a system of 33 second order ordinary differential equations of the form

$$y'' = f(t, y, y'). \quad (8)$$

The system (8) consists of equations of motion for the nine planets, the Moon and three equations for the lunar physical librations. The motion of the Sun is found from the definition of the Solar System barycentre. The equations contain contributions from point-mass interactions, figure effects for Earth and the Moon, Earth tides and perturbations from the five asteroids (1) Ceres, (2) Pallas, (4) Vesta, (7) Iris and (324) Bamberga.

The calculations required for one evaluation of the second derivative for (8) are described in Figure 1. A fuller description is given in [5] and by inference in the program DE118i.ARC of Moshier, available on the internet.

The model equations used in DE102 can be generalised in a number of ways. For example, terms modelling the deformation of the Moon's surface by the Earth and perturbations from other asteroids can be included. However, the model equations of DE102 have proven sufficiently accurate and refinements to DE102 (see, for example [8]) have been in the coordinate systems used, and in the observations used to define the initial conditions and physical constants.

1. Initialise

- a) Calculate the heliocentric position and velocity for the asteroids and transform to approximate barycentric values. These values are corrected once the correct position of the Sun is known.
- b) Calculate the distance between the bodies. The distances involving the Sun or asteroids are estimates only. These distances are corrected once the correct position of the Sun is known.
- c) Use fixed-point iteration to find the correct position and velocity of the Sun and asteroids, then correct the distances involving the Sun or asteroids.
- d) Calculate the cube of the distances between all bodies.

2. Point-mass acceleration

- a) Calculate the Newtonian acceleration of all bodies.
- b) Calculate the post-Newtonian acceleration of the planets and the Moon.

3. Figure of the Moon

- a) Form the rotation matrix for the transformation from space to body coordinates.
- b) Calculate the effect of the point-mass Earth on the lunar figure and add this to the lunar acceleration.
- c) Calculate the torque on the Moon due to the gravitational interaction between the lunar figure and the external point-mass Earth.
- d) The acceleration from b) induces an acceleration in the Earth - add this to the Earth's acceleration.
- e) Calculate the effect of the point-mass Sun on the lunar figure and add this to the lunar acceleration.
- f) Calculate the torque on the Moon due to the gravitational interaction between the lunar figure and the external point-mass Sun.
- g) Calculate the acceleration of the libration angles.

4. Figure of the Earth

- a) Calculate the effect of the point-mass Moon on the Earth's figure and add this to the Earth's acceleration.
- b) The acceleration from a) induces an acceleration in the Moon - add this to the lunar acceleration.
- c) Calculate the contribution to the acceleration of the Moon and the Earth due to the Earth tides.
- d) Calculate the effect of the point-mass Sun on the Earth's figure and add this to the Earth's acceleration.

The accelerations in this section are adjusted for the precession and nutation of the equinox and obliquity of the ecliptic.

Figure 1. A summary of the calculations required for one evaluation of the second derivative in the mathematical model of DE 102.

4. Numerical experiments

We conducted numerical tests of the two new 8-9 pairs and the 7-8 pair of Prince and Dormand on the model equations described in the previous section. The results are illustrated below. The pairs are denoted by PD78 (Prince and Dormand 7-8), P16 (new 16-stage) and P17 (new 17-stage).

A computer which performed quadruple precision in hardware was unavailable and hence we used the the multiprecision Fortran90 package MPFUN90 of Bailey [1], with the precision level set at 35 digits, approximately that of quadruple precision. The multiprecision version of our program was 270 times slower than our double precision version which makes the use of MPFUN90 impractical for long integrations.

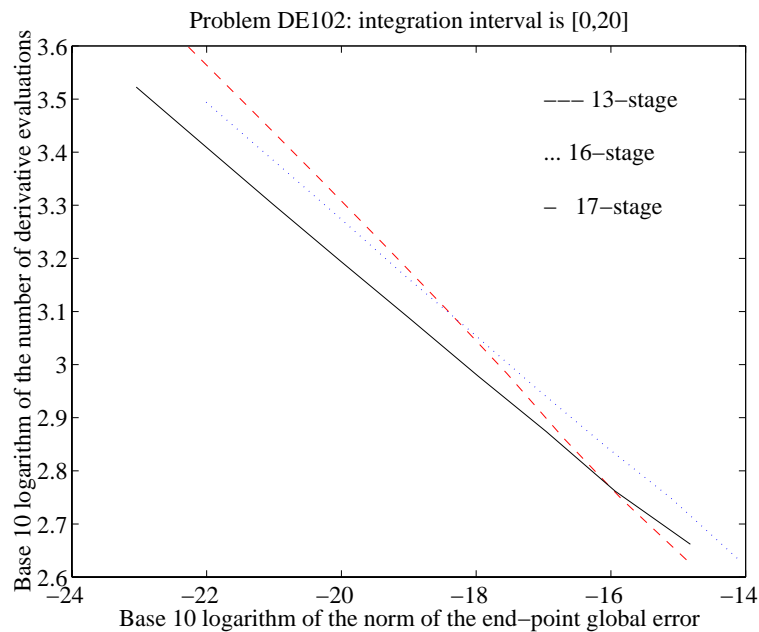


Figure 2. A log-log graph of the number of derivative evaluations against the norm of the end-point global error for DE102 with a integration interval of 20. Prince and Dormand 7-8 pair - dashed line, new 16-stage pair - dotted line, new 17-stage pair - solid line.

The coefficients of the 7-8 pair as specified in [6] are accurate to approximately 18 digits. We recalculated the coefficients in 100 digit arithmetic using the values of the free parameters in [6] and used these coefficients, rounded to 35 digits. The global error in a numerical solution was obtained by calculating a more accurate solution and taking the difference between the two solutions.

The first example is for an integration interval of 20 and local error tolerances of 10^i , $i = -14, \dots, -22$. Figure 2 contains the log-log graph of the number of derivative evaluations against the norm of the end-point global error (the data points have been joined for clarity).

Pair P17 is more efficient than P16 suggesting the efficiency is improved by adding a stage. The gain in efficiency varies from 15 to 20 percent, in good agreement with that predicted using E_{10}^2 . The pairs P16 and P17 are more efficient than PD8 for global errors smaller than (approximately) 10^{-16} , and $10^{-18.5}$ respectively. In addition and as can be expected from the order of the pairs, the efficiency of the 8-9 pairs relative to the 7-8 pair increases as the global error decreases. For example, P17 is 16 percent more efficient for a global error of 10^{-20} and 29 percent more efficient for a global error of 10^{-22} .

The second example is for an integration interval of 50 using the same local error tolerances as in the first example. The results are given in Figure 3. P16 was

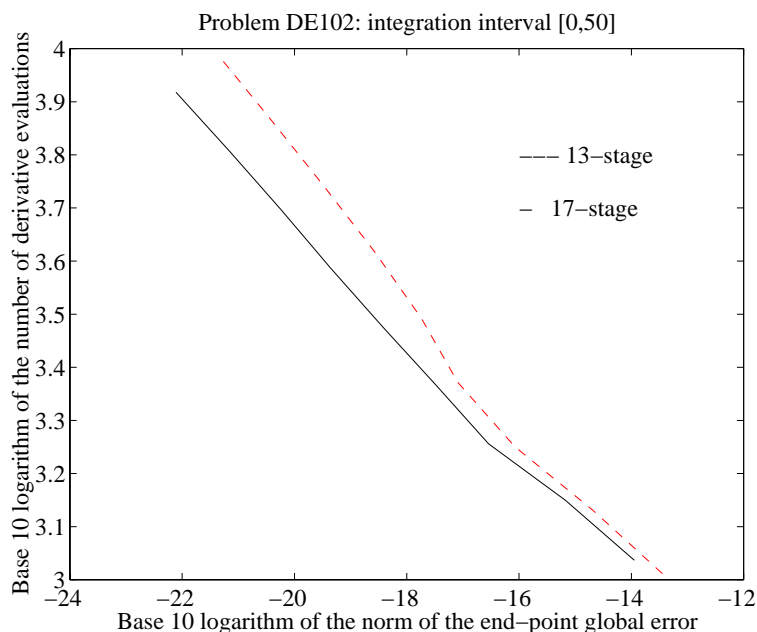


Figure 3. A log-log graph of the number of derivative evaluations against the norm of the end-point global error for DE102 with a integration interval of 50. Prince and Dormand 7-8 pair - dashed line, new 17-stage pair - solid line.

excluded because our test results such as those in Figure 2 showed P16 was less efficient than P17 for the local error tolerances we were using.

The efficiency of P17 relative to PD78 as a function of the global error is similar to that for the first example, except for a minor difference at the larger global errors.

The global errors are larger than in the first example, a result which is consistent with a larger interval of integration.

5. Discussion

The main aim of our work was to investigate if 8-9 explicit Runge-Kutta pairs were more efficient than lower order pairs, principally 7-8 pairs, for numerically integrated ephemerides. We derived a new family of 8-9 pairs, obtained near optimal 8-9 pairs from this family and an existing one, and compared the performance of these pairs and the 7-8 pair of Prince and Dormand on the model equations of the ephemeris DE102.

Our testing showed the 8-9 pairs were usually more efficient than the 7-8 pair. The gain in efficiency was not large, but given the amount of CPU time required to produce ephemerides, the gain is significant. Our testing also showed that near optimal 17-stage 8-9 pairs can be more efficient than near optimal 16-stage 8-9 pairs.

As part of this work we introduced the model equations of DE102 as a test problem for integrators of initial value ordinary differential equations. This problem, in addition to being a realistic one, has several interesting numerical aspects. For example, the position and velocity of the Sun is found by solving a system of nonlinear (algebraic) equations. As in [5], we used fixed point iteration; the question arises as to whether there is a better way to solve the equations.

References

1. D.H. Bailey, *A Fortran-90 based multiprecision System*, RNR Technical Report RNR-94-013, NAS Scientific Computation Branch, NASA Ames Research Center, January, 1995.
2. E. Fehlberg, *Classical fifth-, sixth-, seventh-, and eighth-order Runge-Kutta formulas with step-size control*, NASA Technical Report NASA TR R-287 (1968), 82 pages.
3. E. Hairer, S.P. Nørsett, G. Wanner, *Solving ordinary differential equations I: nonstiff problems*, Springer-Verlag, 1987.
4. S.L. Moshier, *Comparison of a 7000-year lunar ephemeris with analytical theory*, *Astron. Astrophys.* **262** (1982), 613-616.
5. X.X. Newhall, E.M. Standish, J.G. Williams, *DE 102: a numerically integrated ephemeris of the Moon and planets spanning forty-four centuries*, *Astron. Astrophys.* **125** (1983), 150-167.
6. P.J. Prince and J.R. Dormand, *High-order embedded Runge-Kutta formulae*, *J. Comput. Appl. Math.* **7** (1981), 67-76.
7. P.W. Sharp, E. Smart, *Explicit Runge-Kutta pairs with one more derivative evaluation than the minimum*, *SIAM J. Sci. Comput.* **14** (1993), 338-348.
8. E.M. Standish, X.X. Newhall, J.G. Williams, W.F. Folkner, W.F., *JPL Planetary and Lunar Ephemerides, DE403/LE403*, JPL IOM 314.10-127, 1995.
9. J.H. Verner, *Explicit Runge-Kutta methods with estimates of the local truncation error*, *SIAM J. Num. Anal.* **15** (1978), 772-790.
10. J.H. Verner, *A contrast of some Runge-Kutta formula pairs*, *SIAM J. Num. Anal.* **27** (1990), 1332-1344.
11. J.H. Verner, *High order explicit Runge-Kutta pairs with low stage order*, *App. Num. Math.* **22** (1996), 345 - 357.

Special Issue on Models, Methods, and Applications of Dynamics and Control in Engineering Sciences: State of the Art

Call for Papers

Since the current literature on dynamics and control is scattered over a range of journals, books, chapters of books, and a large number of conference proceedings, which are often difficult to obtain, the goal of this special issue of MPE is to present papers, containing complete reviews on dynamics models, available in the current literature, to classify them, and to discuss their applications and limitations. In this special issue, the authors could recommend appropriate models and control criteria for various applications on engineering and sciences and suggest directions for further works. It is also open for critical reviews, open problems, and future developments. Discussions on MEMS and NEMS are also encouraged.

Before submission authors should carefully read over the journal's Author Guidelines, which are located at <http://www.hindawi.com/journals/mpe/guidelines.html>. Prospective authors should submit an electronic copy of their complete manuscript through the journal Manuscript Tracking System at <http://mts.hindawi.com/> according to the following timetable:

Manuscript Due	August 1, 2009
First Round of Reviews	November 1, 2009
Publication Date	February 1, 2010

Lead Guest Editor

Jose Manoel Balthazar, Department of Statistics, Applied Mathematics and Computation, State University of São Paulo at Rio Claro, P.O. Box 178, Rio Claro 13500-230, SP, Brazil; jmbaltha@rc.unesp.br

Guest Editors

Paulo Batista Gonçalves, Civil Engineering Department, Pontifical Catholic University of Rio de Janeiro (PUC-Rio), 22453-900 Rio de Janeiro, RJ, Brazil; paulo@puc-rio.br

Stefano Lenzi, Istituto di Scienza e Tecnica delle Costruzioni, Università Politecnica delle Marche, via Brezze Bianche, Monte D'Ago, Ancona 60131, Italy; lenci@univpm.it

Yuri Vladimirovich Mikhlin, Department of Applied Mathematics, Kharkov Polytechnical Institute, National Technical University, Kharkov 61002, Ukraine; muv@kpi.kharkov.ua

Special Issue on Decision Support for Intermodal Transport

Call for Papers

Intermodal transport refers to the movement of goods in a single loading unit which uses successive various modes of transport (road, rail, water) without handling the goods during mode transfers. Intermodal transport has become an important policy issue, mainly because it is considered to be one of the means to lower the congestion caused by single-mode road transport and to be more environmentally friendly than the single-mode road transport. Both considerations have been followed by an increase in attention toward intermodal freight transportation research.

Various intermodal freight transport decision problems are in demand of mathematical models of supporting them. As the intermodal transport system is more complex than a single-mode system, this fact offers interesting and challenging opportunities to modelers in applied mathematics. This special issue aims to fill in some gaps in the research agenda of decision-making in intermodal transport.

The mathematical models may be of the optimization type or of the evaluation type to gain an insight in intermodal operations. The mathematical models aim to support decisions on the strategic, tactical, and operational levels. The decision-makers belong to the various players in the intermodal transport world, namely, drayage operators, terminal operators, network operators, or intermodal operators.

Topics of relevance to this type of decision-making both in time horizon as in terms of operators are:

- Intermodal terminal design
- Infrastructure network configuration
- Location of terminals
- Cooperation between drayage companies
- Allocation of shippers/receivers to a terminal
- Pricing strategies
- Capacity levels of equipment and labour
- Operational routines and lay-out structure
- Redistribution of load units, railcars, barges, and so forth
- Scheduling of trips or jobs
- Allocation of capacity to jobs
- Loading orders
- Selection of routing and service

Before submission authors should carefully read over the journal's Author Guidelines, which are located at <http://www.hindawi.com/journals/jamds/guidelines.html>. Prospective authors should submit an electronic copy of their complete manuscript through the journal Manuscript Tracking System at <http://mts.hindawi.com/>, according to the following timetable:

Manuscript Due	June 1, 2009
First Round of Reviews	September 1, 2009
Publication Date	December 1, 2009

Lead Guest Editor

Gerrit K. Janssens, Transportation Research Institute (IMOB), Hasselt University, Agoralaan, Building D, 3590 Diepenbeek (Hasselt), Belgium; Gerrit.Janssens@uhasselt.be

Guest Editor

Cathy Macharis, Department of Mathematics, Operational Research, Statistics and Information for Systems (MOSI), Transport and Logistics Research Group, Management School, Vrije Universiteit Brussel, Pleinlaan 2, 1050 Brussel, Belgium; Cathy.Macharis@vub.ac.be

Special Issue on Nonlinear Vibrations, Stability Analysis and Control

Call for Papers

Important advances in mathematics, physics, biology, and engineering science have shown the importance of the analysis of instabilities and strongly coupled dynamical behavior. New investigation tools enable us to better understand the dynamical behavior of more complex structures. However, the increasing interest in mechanical structures with extreme performances has propelled the scientific community toward the search for solution of hard problems exhibiting strong nonlinearities. As a consequence, there is an increasing demand both for nonlinear structural components and for advanced multidisciplinary and multiscale mathematical models and methods. In dealing with the phenomena involving a great number of coupled oscillators, the classical linear dynamic methods have to be replaced by new specific mathematical tools.

This special issue aims to assess the current state of nonlinear structural models in vibration analysis, to review and improve the already known methods for analysis of nonlinear and oscillating systems at a macroscopic scale, and to highlight also some of the new techniques which have been applied to complex structures.

We are looking for original high-quality research papers on topics of interest related to specific mathematical models and methods for nonlinear and strongly coupled (correlated) oscillating systems and for distributed-parameter structures that include but are not limited to the following main topics:

- Vibration analysis of distributed-parameter and multi-body systems, parametric models
- Global methods, wavelet methods, and fractal analysis for spatially and temporally coupled oscillators
- Nonlinear time series methods for dynamic systems
- Control of nonlinear vibrations and bifurcations, control of chaos in vibrating systems. Transient chaos. Chaotic oscillators. Bifurcations
- Micro- and nanovibrating structural systems

Before submission authors should carefully read over the journal's Author Guidelines, which are located at <http://www.hindawi.com/journals/mpe/guidelines.html>. Prospective authors should submit an electronic copy of their complete manuscript through the journal Manuscript Tracking Sys-

tem at <http://mts.hindawi.com/> according to the following timetable:

Manuscript Due	January 1, 2010
First Round of Reviews	April 1, 2010
Publication Date	July 1, 2010

Lead Guest Editor

Carlo Cattani, University of Salerno, Via Ponte Don Melillo, 84084 Fisciano (SA), Italy; ccattani@unisa.it

Guest Editors

Alexander P. Seyranian, Moscow State Lomonosov University, Michurinsky pr. 1, 119192 Moscow, Russia; seyran@imec.msu.ru

Irena Trendafilova, Department of Mechanical Engineering, University of Strathclyde, 75 Montrose Street, Glasgow G1 1XJ, UK; irina.trendafilova@strath.ac.uk