



<http://researchspace.auckland.ac.nz>

ResearchSpace@Auckland

Copyright Statement

The digital copy of this thesis is protected by the Copyright Act 1994 (New Zealand).

This thesis may be consulted by you, provided you comply with the provisions of the Act and the following conditions of use:

- Any use you make of these documents or images must be for research or private study purposes only, and you may not make them available to any other person.
- Authors control the copyright of their thesis. You will recognise the author's right to be identified as the author of this thesis, and due acknowledgement will be made to the author where appropriate.
- You will obtain the author's permission before publishing any material from their thesis.

To request permissions please use the Feedback form on our webpage.

<http://researchspace.auckland.ac.nz/feedback>

General copyright and disclaimer

In addition to the above conditions, authors give their consent for the digital copy of their work to be used subject to the conditions specified on the [Library Thesis Consent Form](#) and [Deposit Licence](#).

Note : Masters Theses

The digital copy of a masters thesis is as submitted for examination and contains no corrections. The print copy, usually available in the University Library, may contain corrections made by hand, which have been requested by the supervisor.

Powering Implantable Devices from a Surface

With Application to Physiological Monitoring in Mice

Daniel McCormick

Supervised by: **Dr. David Budgett, Associate Professor Patrick Hu and Associate Professor Poul Nielsen**

A thesis submitted in partial fulfilment of the requirements for the degree of

Doctor of Philosophy in Bioengineering

The University of Auckland, New Zealand

2011

Abstract

Magnetic fields offer the prospect of transferring energy through the skin to power active implantable devices for indefinite periods of time. Inductive power transfer is an attractive technology for smart implantable devices to overcome limitations of batteries and avoid the infection risk associated with direct electrical connections. This thesis presents work addressing the problem of powering implantable devices for monitoring the physiological status of laboratory mice.

Although the fundamental principles for transferring power inductively are very well understood, there are many practical issues to be resolved when transferring power over a variable air gap. A typical mouse is only 20 grams in body weight, and a key aspect to miniaturising a telemetry system is the elimination of an internal battery. This necessitates an inductive power link capable of continuously supplying power as the mouse moves freely within the confines of its home cage. An inductive power link involves a primary inductive coil outside the animal, and a secondary coil located inside the animal. To accommodate the mouse application, the link must operate when the secondary has an arbitrary orientation and location with respect to the primary. To solve this problem, a planar winding structure is proposed that is placed under the cage of the animal. Advantages of a planar structure over cage encompassing primary coil structures include proximity to the animal, more uniform magnetic coupling and scalability to cover different size cages.

Development of this system resulted in an analytical method of determining which one of arbitrary number of independently located primary coils can transfer power to an arbitrarily oriented pickup with the greatest efficiency. A consequence of the analysis was the development of a method of optimising the primary and pickup structures in isolation from each other. This method was developed for the arbitrary coupling problem but is applicable to any loosely coupled inductive link – including those which utilise a ferromagnetic pickup core.

The thesis concludes with the implementation and evaluation of a prototype inductive link for powering an arbitrarily oriented implant. Results from the prototype are compared to predictions based on the analyses developed. The agreement of results validates the proposed methods and confirms that a planar winding structure is capable of continuously powering an arbitrarily oriented implant.

TABLE OF CONTENTS

| | | |
|----------|--|-----------|
| 1 | INTRODUCTION | 1 |
| 1.1 | TELEMETRY AS A TOOL FOR PHYSIOLOGICAL MONITORING | 1 |
| 1.1.1 | <i>Advantages of Telemetry</i> | 2 |
| 1.1.2 | <i>Caveats of Telemetry</i> | 4 |
| 1.1.3 | <i>Summary</i> | 5 |
| 1.2 | APPLICATION OF INDUCTIVE POWER TRANSFER TO PHYSIOLOGICAL MONITORING..... | 5 |
| 1.2.1 | <i>Wireless Power and Telemetry</i> | 5 |
| 1.2.2 | <i>A Historical Perspective on Inductive Power Transfer</i> | 7 |
| 1.2.3 | <i>Energy Storage and Miniaturisation</i> | 9 |
| 1.3 | POWERING AN ARBITRARILY ORIENTED PICKUP | 10 |
| 1.3.1 | <i>Differences between Small Animal Monitoring and Industrial ICPT</i> | 10 |
| 1.3.2 | <i>Powered Volume</i> | 10 |
| 1.3.3 | <i>Limitations of Unidirectional System</i> | 11 |
| 1.4 | REVIEW OF USING MULTIPLE PRIMARIES | 13 |
| 1.4.1 | <i>Continuous Operation</i> | 14 |
| 1.4.2 | <i>Magnitude Based Control of Excitation</i> | 15 |
| 1.4.3 | <i>Frequency Control of Excitation</i> | 16 |
| 1.4.4 | <i>Discontinuous Operation</i> | 16 |
| 1.4.5 | <i>Field Steering</i> | 18 |
| 1.5 | REVIEW OF USING MULTIPLE PICKUPS..... | 18 |
| 1.5.1 | <i>Combination of Multiple Primaries and Secondaries</i> | 20 |
| 1.6 | PLANAR WINDING STRUCTURE | 21 |
| 1.6.1 | <i>Comparison of Existing and Proposed Techniques</i> | 22 |
| 1.6.2 | <i>Usefulness of Existing Techniques for a Mouse Telemeter</i> | 24 |
| 1.6.3 | <i>Control and Excitation</i> | 25 |
| 1.7 | PURPOSE AND SCOPE | 27 |
| 2 | INDUCTIVE LINK ANALYSIS AND POWER TRANSFER CAPABILITY | 31 |
| 2.1 | INTRODUCTION | 31 |
| 2.2 | POWER TRANSFER CAPABILITY | 32 |
| 2.2.1 | <i>Fundamentals</i> | 32 |
| 2.3 | TUNING..... | 33 |
| 2.3.1 | <i>Loosely Coupled Vs Industrial/Consumer ICPT</i> | 34 |
| 2.3.2 | <i>Maximum Power Transfer</i> | 35 |
| 2.3.3 | <i>Impedance Matching To Achieve Maximum Power Transfer</i> | 37 |
| 2.4 | BANDWIDTH AND POWER TRANSFER | 41 |

| | | |
|----------|---|-----------|
| 2.5 | NEW FIGURES OF MERIT FOR LOOSELY COUPLED ICPT | 43 |
| 2.5.1 | Vector Form of B_0 , A_c , X_1 and X_2 | 45 |
| 2.5.2 | Relationship of B_0 to Mutual Inductance and k | 47 |
| 2.6 | EXAMPLE APPLICATION OF X_1 , X_2 , B_0 AND A_c | 47 |
| 2.6.1 | Example 1: Predict Power Transfer of Two Ferrite Pickups..... | 47 |
| 2.6.2 | Example 2: Increase Powered Area of an Existing System..... | 50 |
| 2.6.3 | Concluding Remarks on the Application of X_1 and X_2 | 56 |
| 2.7 | OPERATING OFF MAXIMUM POWER TRANSFER..... | 56 |
| 2.7.1 | Secondary Efficiency | 57 |
| 2.7.2 | Reduction of Power Transferred | 58 |
| 2.7.3 | Summary of the Effect of Operating off Maximum Power Transfer | 60 |
| 2.8 | TRANSIENT ANALYSIS UTILISING CONSTANT Q | 61 |
| 2.8.1 | Primary Transient Response | 62 |
| 2.8.2 | Pickup Transient Response..... | 63 |
| 2.8.3 | Link Transient Response..... | 65 |
| 2.8.4 | Transient Analysis and Constant Q..... | 66 |
| 2.8.5 | Filter Capacitance | 68 |
| 2.9 | QUALITY FACTOR AND POWER TRANSFER | 68 |
| 2.10 | USEFUL RELATIONSHIPS FOR LOOSELY COUPLED LINKS..... | 69 |
| 2.11 | SUMMARY | 71 |
| 3 | ANALYSIS OF A PLANAR WINDING STRUCTURE FOR POWERING ARBITRARILY ORIENTATED | |
| | IMPLANTABLE DEVICES | 73 |
| 3.1 | INTRODUCTION | 73 |
| 3.2 | PARAMETERS TO OPTIMISE | 74 |
| 3.3 | FIELD GENERATION..... | 75 |
| 3.4 | COIL ESR..... | 79 |
| 3.4.1 | DC Resistance..... | 79 |
| 3.4.2 | Skin Effect | 80 |
| 3.4.3 | Single Turn Equivalent Values..... | 81 |
| 3.4.4 | Eddy Current Losses | 84 |
| 3.4.5 | Self Inductance..... | 92 |
| 3.5 | DETERMINING MINIMUM COUPLING | 93 |
| 3.5.1 | Formulation of the Problem..... | 93 |
| 3.5.2 | Minimum B_0 for 3 Coils | 94 |
| 3.6 | EXTENDING MINIMUM POWER ANALYSIS TO N COILS | 97 |
| 3.6.1 | Iterative Method for N Coils Based on 3 Coil Method..... | 97 |
| 3.6.2 | Geometric Solution Based On Convex Hull Problem | 99 |

| | | |
|----------|---|------------|
| 3.6.3 | <i>Field Data for Use with These Algorithms</i> | 103 |
| 3.6.4 | <i>Optimisation of Winding Geometry</i> | 103 |
| 3.6.5 | <i>Fill Factor, Size and B_{0-Min}</i> | 104 |
| 3.6.6 | <i>Comparison of Arbitrarily Orientated and Unidirectional ICPT</i> | 106 |
| 3.6.7 | <i>Fill Factor, Size and X_1</i> | 108 |
| 3.6.8 | <i>X_1 in the Presence of Eddy Currents</i> | 109 |
| 3.6.9 | <i>Coil Q</i> | 111 |
| 3.6.10 | <i>Switch Voltage</i> | 113 |
| 3.7 | GENERAL DESIGN PROCEDURE..... | 115 |
| 3.7.1 | <i>Case 1: Unlimited Copper without Eddy Currents</i> | 115 |
| 3.7.2 | <i>Case 2: Low Frequency PCB Winding</i> | 116 |
| 3.7.3 | <i>Case 3: High Frequency PCB Winding (Eddy Current Limited)</i> | 116 |
| 3.7.4 | <i>A Practical Design Flow</i> | 117 |
| 3.8 | PRACTICAL CONSIDERATIONS..... | 118 |
| 3.8.1 | <i>Orientation of Worst Coupling</i> | 118 |
| 3.8.2 | <i>Edge Effects</i> | 118 |
| 3.9 | B0 CHARTS FOR PRIMARIES COMPOSED OF RECTANGULAR AND SQUARE COILS..... | 120 |
| 3.9.1 | <i>Square Four Layer</i> | 121 |
| 3.9.2 | <i>Rectangular Four Layer</i> | 122 |
| 3.9.3 | <i>Two Layer Square</i> | 123 |
| 3.9.4 | <i>Four Layer Square with Fill Factor of One</i> | 124 |
| 3.10 | SUMMARY..... | 126 |
| 4 | DETERMINATION OF MUTUAL INDUCTANCE IN LOOSELY COUPLED LINKS BY FINITE ELEMENT ANALYSIS | 127 |
| 4.1 | INTRODUCTION..... | 127 |
| 4.2 | SIMPLIFIED ANALYSIS OF COUPLING INCLUDING MAGNETIC MATERIALS AND DISTRIBUTED WINDINGS..... | 129 |
| 4.2.1 | <i>Self Inductance</i> | 132 |
| 4.3 | FINITE ELEMENT METHOD WITH VERY LOOSELY COUPLED SYSTEMS..... | 133 |
| 4.3.1 | <i>Extracting Inductances from the Finite Element Model</i> | 134 |
| 4.3.2 | <i>Surface Integrals of Flux</i> | 134 |
| 4.3.3 | <i>Energy Based Calculation</i> | 135 |
| 4.4 | CONVERTING TO A_e AND μ_{CORE} | 137 |
| 4.4.1 | <i>Fluxmetric μ_{CORE}</i> | 138 |
| 4.4.2 | <i>Magnetometric μ_{CORE}</i> | 138 |
| 4.4.3 | <i>Self Inductance</i> | 139 |
| 4.5 | PARTIAL VOLUME MODEL OF INDUCTIVE LINKS..... | 140 |
| 4.5.1 | <i>Boundary Conditions</i> | 142 |

| | | |
|----------|---|------------|
| 4.5.2 | <i>Interpreting Partial Volume Results in Terms of A_e and μ_{core}</i> | 143 |
| 4.5.3 | <i>Example Calculation with a Sub Volume Model</i> | 143 |
| 4.6 | FINITE ELEMENT MODEL FOR EVALUATING PICKUP GEOMETRY INDEPENDENT OF THE PRIMARY | 145 |
| 4.6.1 | <i>3D Model of Pickup in Constant Field</i> | 145 |
| 4.7 | DETERMINING M_{CORE} AND A_e | 148 |
| 4.7.1 | <i>Verification that Mutual Energy is Localised in the Region of the Pickup</i> | 149 |
| 4.8 | CHARTS OF μ_{CORE} FOR RODS..... | 151 |
| 4.8.1 | <i>Comparison with Published Data</i> | 154 |
| 4.8.2 | <i>Empirical Model of μ_{core} for Rods</i> | 155 |
| 4.8.3 | <i>Comparison of Rods with Oblate and Prolate Spheroids</i> | 156 |
| 4.9 | CALCULATIONS OF μ_{CORE} FOR PRACTICAL GEOMETRIES | 157 |
| 4.9.1 | <i>Effect of Aspect Ratio on A_e and μ_{core}</i> | 160 |
| 4.10 | SUMMARY | 162 |
| 5 | DEVELOPMENT OF A WIRELESS POWER SUPPLY FOR AN IMPLANTABLE MOUSE TELEMETER..... | 165 |
| 5.1 | INTRODUCTION | 165 |
| 5.2 | EXPERIMENTAL SYSTEM OVERVIEW..... | 166 |
| 5.2.1 | <i>Power Requirements</i> | 166 |
| 5.2.2 | <i>System Components</i> | 167 |
| 5.3 | EXPERIMENTAL SYSTEM DESIGN | 170 |
| 5.3.1 | <i>Choice of Primary Coil Geometry</i> | 170 |
| 5.3.2 | <i>Pickup Coil</i> | 173 |
| 5.3.3 | <i>Power Conditioning Circuitry</i> | 176 |
| 5.3.4 | <i>Telemeter Construction</i> | 177 |
| 5.3.5 | <i>Switching Circuitry</i> | 178 |
| 5.3.6 | <i>Switch Implementation</i> | 179 |
| 5.4 | EXPERIMENTAL POWER TRANSFER MEASUREMENTS | 180 |
| 5.4.1 | <i>Measurement Rig</i> | 181 |
| 5.4.2 | <i>Power Transfer Capability</i> :..... | 183 |
| 5.5 | TRANSIENT PERFORMANCE..... | 185 |
| 5.5.1 | <i>Switching Time</i> | 185 |
| 5.5.2 | <i>Power Conditioning Circuitry</i> | 186 |
| 5.6 | CONTINUOUSLY POWERING AN IMPLANT: | 187 |
| 5.6.1 | <i>Measurement Method</i> | 187 |
| 5.6.2 | <i>Results</i> | 187 |
| 5.7 | DISCUSSION | 189 |
| 5.8 | FUTURE WORK | 189 |
| 5.8.1 | <i>Detecting Power Level</i> | 189 |

| | | |
|--------------------|--|------------|
| 5.8.2 | <i>Topology based Coil Searching</i> | 190 |
| 5.8.3 | <i>Detuning the Pickup</i> | 190 |
| 5.9 | CONCLUSIONS | 191 |
| 6 | FREQUENCY RESPONSE OF IMPLANTABLE BLOOD PRESSURE TELEMTRY SYSTEMS | 193 |
| 6.1 | INTRODUCTION | 193 |
| 6.2 | BACKGROUND | 194 |
| 6.3 | MATERIALS AND METHODS..... | 195 |
| 6.4 | TEST SYSTEM FOR MEASURING HIGH BANDWIDTH PRESSURE SENSOR OPERATION. | 196 |
| 6.4.1 | <i>System Overview</i> | 196 |
| 6.4.2 | <i>Measurement Bandwidth</i> | 198 |
| 6.5 | FREQUENCY RESPONSES OF COMMERCIAL TELEMETERS | 200 |
| 6.6 | IMPORTANCE OF GEL VOLUME..... | 206 |
| 6.7 | TESTING CONSEQUENCES OF TIP REMOVAL | 209 |
| 6.8 | SIMULATED DYNAMIC PERFORMANCE | 210 |
| 6.8.1 | <i>Transfer Function Identification</i> | 211 |
| 6.8.2 | <i>Simulated Results</i> | 212 |
| 6.9 | DISCUSSION | 216 |
| 6.9.1 | <i>Power Consumption and Frequency Response</i> | 217 |
| 6.9.2 | <i>Limitations</i> | 217 |
| 6.10 | CONCLUSIONS..... | 218 |
| 7 | CONCLUSIONS | 219 |
| 7.1 | SUMMARY | 219 |
| 7.1.1 | <i>Rational</i> | 219 |
| 7.1.2 | <i>Method</i> | 220 |
| 7.1.3 | <i>Result</i> | 222 |
| 7.2 | CONTRIBUTIONS | 223 |
| 7.3 | PUBLICATIONS | 224 |
| 7.3.1 | <i>Journal Papers</i> | 224 |
| 7.3.2 | <i>Conference Papers</i> | 225 |
| 7.3.3 | <i>Conference Abstracts and Posters</i> | 225 |
| 7.4 | FUTURE RESEARCH DIRECTION..... | 226 |
| 8 | REFERENCES | 227 |
| APPENDIX A: | MATLAB CODE FOR DETERMINING MINIMUM COUPLING | 235 |
| A.1 | CONVEX HULL BASED FUNCTION FOR DETERMINING MINIMUM COUPLING | 235 |
| A.2 | SUB FUNCTIONS | 236 |
| A.3 | EXAMPLE PROGRAM FOR DETERMINING MINIMUM COUPLING | 237 |

| | | |
|--------------------|--------------------------------------|------------|
| A.4 | SUB FUNCTIONS FOR EXAMPLE CODE | 239 |
| APPENDIX B: | AC SWITCH..... | 241 |
| B.1 | INTRODUCTION | 241 |
| B.2 | OPERATION..... | 241 |

LIST OF FIGURES

| | |
|--|----|
| FIGURE 1-1 A TELEMETRY SYSTEM FOR SMALL ANIMAL MONITORING SHOWING TWO ANIMALS AND RECEIVERS. THIS (TELEMETRY RESEARCH LTD) SYSTEM INCLUDES A WIRELESS BATTERY RECHARGER WHICH IS ATYPICAL OF COMMERCIAL SYSTEMS (ADINSTRUMENTS, RETRIEVED 4/5/2010)..... | 2 |
| FIGURE 1-2 A COMMERCIALY AVAILABLE TELEMETER FOR THE CHRONIC RECORDING OF BLOOD PRESSURE AND SYMPATHETIC NERVE ACTIVITY MANUFACTURED BY TELEMETRY RESEARCH LTD. EVIDENT IS THE PROPORTION OF THE TOTAL IMPLANT VOLUME CONSUMED BY THE BATTERY AND CHARGE MANAGEMENT CIRCUITRY..... | 9 |
| FIGURE 1-3 AREA OVER WHICH THE ANIMAL WILL ROAM AND THE HEIGHT THAT THE PICKUP CAN BE EXPECTED TO BE ABOVE THE CHARGING SURFACE DETERMINE THE VOLUME IN WHICH POWER MUST BE AVAILABLE. | 11 |
| FIGURE 1-4 PERCENT OF TIME WHERE THE TELEMETER WAS POWERED INDUCTIVELY IN A UNIDIRECTIONAL SYSTEM OVER A 5 DAY PERIOD..... | 12 |
| FIGURE 1-5 SCHUDER’S ORIGINAL COIL LAYOUT FROM 1963 IN USE ON A 2M X 2M X 2M CAGE(SCHUDER JC, 1963). | 13 |
| FIGURE 1-6 LEFT: A RECTANGULAR HELMHOLTZ PAIR. RIGHT: AN ARRANGEMENT OF HELMHOLTZ PAIRS TO CREATE AN OMNIDIRECTIONAL INDUCTIVE LINK..... | 14 |
| FIGURE 1-7 AN EXAMPLE OF DISCONTINUOUS OPERATION OF AN OMNIDIRECTIONAL LINK (Si, 2008) | 17 |
| FIGURE 1-10A THREE SPATIALLY DISTINCT PICKUP COILS WHICH UTILISE FERRITE CORES (Si, 2008)..... | 19 |
| FIGURE 1-10 THREE ORTHOGONAL AIR CORED PICKUP COILS ARRANGED IN A CONCENTRIC FASHION. AIR SPACE IS UTILISED TO HOUSE THE RECTIFICATION AND FILTERING (LENAERTS AND PUERS, 2006). | 19 |
| FIGURE 1-10 THREE CONCENTRIC WINDINGS ARRANGED AROUND A FERRITE CORE (RYU ET AL., 2007)..... | 19 |
| FIGURE 1-11 A PLANAR SPIRAL COIL SHOWING REGIONS WHERE THE DIRECTION OF THE MAGNETIC FIELD ABOVE IT PREDOMINANTLY FOLLOWS ONE OF THE THREE AXES. | 21 |
| FIGURE 1-12 AN EXPLODED VIEW OF A FOUR LAYER ARRANGEMENT OF COILS WHICH OVERLAPS THE AFOREMENTIONED REGIONS SUCH THAT POWER IS AVAILABLE IN ANY ORIENTATION..... | 22 |
| FIGURE 1-13 FIELD STRENGTH NORMAL TO A SQUARE COIL’S SURFACE..... | 23 |
| FIGURE 1-14 FIELD STRENGTH PARALLEL TO THE SURFACE OF RECTANGULAR COIL..... | 24 |
| FIGURE 2-1 A BASIC ICPT SYSTEM USED TO TRANSFER ENERGY ACROSS A TISSUE BARRIER (Si, 2008). | 32 |
| FIGURE 2-2 SERIES AND PARALLEL TUNING THE PICKUP. ADAPTED FROM (Si, 2008)..... | 34 |
| FIGURE 2-3 SERIES AND PARALLEL TUNING OF A PICKUP WHICH INCLUDES PARASITIC RESISTANCE. | 35 |
| FIGURE 2-4 EFFECT OF COIL IMPEDANCE ON POWER TRANSFER..... | 37 |
| FIGURE 2-5 TWO COILS OF IDENTICAL DIMENSIONS AND COPPER VOLUME WITH DIFFERENT NUMBERS OF TURNS..... | 40 |
| FIGURE 2-6 EQUIVALENT CIRCUIT OF A LOOSELY COUPLED INDUCTIVE LINK WHERE MUTUAL INDUCTANCE HAS BEEN REPLACED WITH AT CURRENT CONTROLLED VOLTAGE SOURCE. AT RESONANCE L_2 AND C_2 CANCEL EACH OTHER LEAVING ONLY THE RESISTIVE ELEMENTS. | 44 |
| FIGURE 2-7 TWO FERRITE CORE PICKUPS..... | 48 |
| FIGURE 2-8 PUSH-PULL INVERTER AND RESONANT TANK WHICH IS FORMED FROM THE PRIMARY WINDING AND A TUNING CAPACITOR – ADAPTED FROM (Si, 2008) | 51 |

| | |
|--|----|
| FIGURE 2-9 PARALLEL ARRANGEMENT OF THREE SPIRALLED RECTANGULAR COILS WHICH ARE DESIGNED TO INCREASE THE POWERED AREA WITHOUT INCREASING THE POWER SUPPLY VOLTAGE. ON THE LEFT IS THE TOP SIDE WHICH IS PLACED NEAREST TO THE ANIMAL. ON THE RIGHT IS THE UNDERSIDE..... | 52 |
| FIGURE 2-10 B_0/L_0 FOR THE EXISTING COIL WITH DIMENSIONS OF 165 BY 125MM..... | 53 |
| FIGURE 2-11 B_0/L_0 FOR INCREASING WIDTHS OF SPIRALLED PRIMARY WINDINGS. WINDING VERTICAL LENGTH IS 34CM OVERALL IN ALL CASES..... | 54 |
| FIGURE 2-12 EXPERIMENTAL DATA FROM EXISTING AND EXPANDED-AREA WIRELESS POWER PAD | 55 |
| FIGURE 2-13 EFFECT OF THE NUMBER OF TURNS ON POWER TRANSFERRED AND SECONDARY EFFICIENCY FOR SERIES AND PARALLEL PICKUPS. | 61 |
| FIGURE 2-14. MODELLING THE TRANSIENT RESPONSE OF THE INDUCTIVE LINK. (A) AC EQUIVALENT CIRCUIT MODEL OF INDUCTIVE LINK. (B) PRIMARY CIRCUIT DC EQUIVALENT MODEL. (C) SECONDARY DC EQUIVALENT MODEL. (D) COUPLED TRANSIENT MODEL. | 63 |
| FIGURE 2-15 RESPONSE TIME AND POWER TRANSFER CAPABILITY AS A FUNCTION OF β FOR A SERIES RESONANT PICKUP. AT MAXIMUM POWER TRANSFER, WHEN $R_{L0} = R_{20}$, RESPONSE TIME IS HALF THE UNLOADED CASE. | 67 |
| FIGURE 3-1 DIMENSIONS OF THE RECTANGULAR WIRE LOOP AND APPROXIMATION OF A SPIRAL COIL WITH NESTED LOOPS..... | 75 |
| FIGURE 3-2 MAGNETIC FIELD STRENGTH B_{0x} , B_{0y} AND B_{0z} 3CM ABOVE A 100MM OUTSIDE DIAMETER -- 50MM INSIDE DIAMETER SPIRAL WINDING. | 78 |
| FIGURE 3-3 SPIRAL COIL OF DIAMETER D_0 , TRACK WIDTH W , TRACK SPACING S AND COPPER THICKNESS T_c | 79 |
| FIGURE 3-4 R_{10} AS A FUNCTION OF FILL FACTOR FOR SPIRAL COILS WITH LINES FOR DIFFERENT RATIOS D_{02}/D_{01} | 82 |
| FIGURE 3-5 INFLUENCE OF TRACK SPACE ON R_{10} | 84 |
| FIGURE 3-6 EDDY CURRENTS INCREASE ESR THROUGH LOSS DUE TO CIRCULATING CURRENTS IN THE PCB TRACKS. | 85 |
| FIGURE 3-7 R_1 , R_{1-DC} AND R_E AS A FUNCTION OF N_1 | 87 |
| FIGURE 3-8 POWER DISSIPATED IN THE PRIMARY WHEN DELIVERING CONSTANT POWER TO THE LOAD. | 88 |
| FIGURE 3-9 THE EFFECT OF TRACK SPACING ON COIL RESISTANCE WHEN EDDY CURRENTS ARE CONSIDERED..... | 89 |
| FIGURE 3-10 TOTAL RESISTANCE R_1 , DC RESISTANCE R_{DC} AND EDDY CURRENT RESISTANCE R_E FOR A 100MM DIAMETER SQUARE COIL WITH A FILL FACTOR OF 0.5 AT 600KHZ,..... | 90 |
| FIGURE 3-11 SINGLE TURN EQUIVALENT RESISTANCE R_{10} , DC RESISTANCE R_{10-DC} AND EDDY CURRENT RESISTANCE R_{E0} FOR THE COIL ABOVE..... | 91 |
| FIGURE 3-12 MINIMUM COUPLING FOR THE CASE OF 3 ORTHOGONAL UNIT VECTORS. LINE MINIMA OCCUR WHEN TWO OF THE VECTORS' MAGNITUDES ARE EQUAL. POINT MINIMA OCCUR WHEN THE MAGNITUDE OF ALL THREE VECTORS ARE EQUAL. | 95 |
| FIGURE 3-13 FINDING DIRECTION OF MINIMUM COUPLING IN 2D | 96 |
| FIGURE 3-14 FLOW DIAGRAM OF THE ITERATIVE METHOD OF DETERMINING MINIMUM COUPLING FOR N COILS | 98 |
| FIGURE 3-15 ITERATIVE METHOD OF CALCULATING B_{0-MIN} BASED ON 3 COIL MINIMUM COUPLING SOLUTION. | 98 |
| FIGURE 3-16 A CONVEX HULL PROBLEM IN 2D | 99 |
| FIGURE 3-17 ADDING ANOTHER VECTOR TO THE SET DIVIDES THE EXISTING SURFACE (A) INTO THREE NEW TRIANGULAR FACETS (B) IF IT EXTENDS BEYOND THE SURFACE. EACH OF THE NEW FACETS COULD LEAD TO A COUPLING MINIMUM. IF THE NEW VECTOR FALLS BELOW THE SURFACE IT CANNOT CONTRIBUTE TO THE WORST CASE COUPLING AS ONE OF THE EXISTING | |

| | |
|---|-----|
| VECTORS WILL PROVIDE MORE POWER. (c) FOR AN ARBITRARY NUMBER OF FIELD VECTORS, THE POSSIBLE MINIMUMS CAN BE FOUND BY FINDING THE CONVEX HULL WHICH ENCLOSES THE SET OF VECTORS. | 100 |
| FIGURE 3-18 SEQUENCE OF OPERATIONS TO CALCULATE B_0 USING CONVEX HULL METHOD. NOTE THAT THE ALGORITHM HAS ONLY ONE LOOP AS OPPOSED TO FIGURE 3-15 WHERE TWO LEVELS OF ITERATION ARE REQUIRED. | 101 |
| FIGURE 3-19 B_0 FOR A 4 LAYER PCB WITH LAYOUT AS SHOWN IN FIGURE 3-34. THE TOP LAYER IS PLOTTED BELOW TO PROVIDE A REFERENCE OF THE EXTENT OF THE PAD. | 102 |
| FIGURE 3-20 B_{0_MIN} AS A FUNCTION OF FILL FACTOR AND COIL DIAMETER FOR THE FOUR LAYER SQUARE GEOMETRY AT A HEIGHT OF 10MM ABOVE THE PAD. | 105 |
| FIGURE 3-21 B_{0_MIN} AS A FUNCTION OF FILL FACTOR AND COIL DIAMETER FOR THE FOUR LAYER SQUARE GEOMETRY AT A HEIGHT OF 30MM ABOVE THE PAD. NOTE THE DIFFERENT B_{0_MIN} SCALE WHEN COMPARED TO FIGURE 3-20. | 105 |
| FIGURE 3-22 B_{0_MIN} AS A FUNCTION OF FILL FACTOR AND COIL DIAMETER FOR THE FOUR LAYER SQUARE GEOMETRY AT A HEIGHT OF 50MM ABOVE THE PAD. NOTE THE DIFFERENT B_{0_MIN} SCALE WHEN COMPARED TO FIGURE 3-20. | 106 |
| FIGURE 3-23 GEOMETRY OF THE PRIMARY COIL UNDER CONSIDERATION FOR A UNIDIRECTIONAL INDUCTIVE LINK. | 107 |
| FIGURE 3-24 FIELD STRENGTH AS A FUNCTION OF DIMENSION A FOR THE UNIDIRECTIONAL INDUCTIVE LINK. | 108 |
| FIGURE 3-25 PRIMARY LINK POTENTIAL X_1 FOR THE FOUR LAYER SQUARE COIL LAYOUT AS A FUNCTION OF FILL FACTOR AND COIL OUTSIDE DIAMETER. | 109 |
| FIGURE 3-26 PRIMARY LINK POTENTIAL X_1 WITH THE NUMBER OF TURNS SET TO MINIMISE R_{10} IN THE PRESENCE OF EDDY CURRENT LOSSES. | 110 |
| FIGURE 3-27 OPTIMUM NUMBER OF TURNS TO MINIMISE R_{10} WHEN EDDY CURRENT LOSSES ARE CONSIDERED AT 600kHz. | 111 |
| FIGURE 3-28 L_{10} AS A FUNCTION OF FILL FACTOR AND SIZE FOR SQUARE SPIRAL COILS. | 112 |
| FIGURE 3-29 FLUX CANCELATION REDUCES SELF INDUCTANCE FOR DISTRIBUTED COILS. | 112 |
| FIGURE 3-30 QUALITY FACTOR AS A FUNCTION OF FILL FACTOR AND DIAMETER. | 113 |
| FIGURE 3-31 RELATIONSHIP BETWEEN RESONANT VOLTAGE (COIL SELECTION SWITCH VOLTAGE RATING) AND POWER TRANSFER. | 115 |
| FIGURE 3-32 DIRECTION OF MINIMUM B_0 FOR FOUR LAYER SQUARE WINDING. UPPER LEFT: ABSOLUTE VALUE OF X COMPONENT OF MINIMUM B_0 DIRECTIONAL VECTOR P . UPPER RIGHT: Y COMPONENT OF P . LOWER LEFT: Z COMPONENT OF P . LOWER RIGHT: MAGNITUDE OF THE PROJECTION OF P ONTO THE X-Y PLANE. | 119 |
| FIGURE 3-33 B_{0_MIN} OVER THE SURFACE OF THE FOUR COIL SQUARE LAYOUT AT A HEIGHT OF 30MM. THE TOP LAYER OF THE WINDING IS PLOTTED TO SHOW THE EXTENT OF THE COVERAGE. | 120 |
| FIGURE 3-34 SQUARE FOUR LAYER COIL LAYOUT. | 121 |
| FIGURE 3-35 B_{0_MIN} FOR FOUR LAYERS OF SQUARE COILS. | 121 |
| FIGURE 3-36 RECTANGULAR FOUR LAYER COIL LAYOUT. | 122 |
| FIGURE 3-37 FOUR LAYER RECTANGULAR WINDING. THE COIL DIAMETER (OD) IS TAKEN TO BE THE EXTERIOR DIMENSION OF THE COIL AS THIS DIMENSION HAS THE GREATEST BEARING ON PERFORMANCE. | 123 |
| FIGURE 3-38 TWO LAYER SQUARE LAYOUT. | 123 |
| FIGURE 3-39 TWO LAYER SQUARE COIL LAYOUT. | 124 |
| FIGURE 3-40 FOUR LAYER SQUARE COIL LAYOUT. | 124 |
| FIGURE 3-41 SQUARE FOUR LAYER 'FULL WINDING' (FILL FACTOR = 1). | 125 |

| | |
|--|-----|
| FIGURE 4-1 A_E IS THE EQUIVALENT SURFACE AREA WHICH REPRESENTS THE FLUX “CAPTURING ABILITY” OF A DISTRIBUTED OR FERROMAGNETIC PICKUP. WHEN PLACED IN A CONSTANT MAGNETIC FIELD IT RECEIVES THE SAME FLUX LINKAGES..... | 129 |
| FIGURE 4-2 RELATIONSHIP BETWEEN μ_{core} , A_c AND A_E FOR VARIOUS COMBINATIONS OF CONDUCTOR VOLUME AND SOFT MAGNETIC MATERIALS..... | 130 |
| FIGURE 4-3 μ_{core} AS A FUNCTION OF μ_r FOR A MODEL OF A WÜRTH ELEKTRONIK 744772220 | 131 |
| FIGURE 4-4 THE EFFECT OF A HIGH PERMEABILITY MATERIAL ON THE MAGNETIC FIELD DISTRIBUTION OF AN OPEN MAGNETIC COMPONENT. | 133 |
| FIGURE 4-5 EXAMPLES OF APPROPRIATE BOUNDARY CONDITIONS WHEN THE SOURCE FIELD EXIST OUTSIDE THE DOMAIN | 142 |
| FIGURE 4-6 GEOMETRY OF SOLENOID OF EQUATION 4–21 | 146 |
| FIGURE 4-7 SCHEMATIC OF THE FINITE ELEMENT MODEL FOR GENERATING A CONSTANT MAGNETIC FIELD USING A SOLENOID. | 146 |
| FIGURE 4-8 PLOT SHOWING UNIFORMITY OF B_z WITH DOMAIN LENGTH EQUAL TO THE SOLENOID’S LENGTH DIVIDED BY A 1000 AND RADIUS EQUAL TO THE SOLENOID’S RADIUS DIVIDED BY 10 | 147 |
| FIGURE 4-9 B_z AS A FUNCTION OF RADIAL DISTANCE FOR VARIOUS DISTANCES FROM THE CENTRE OF THE ROD. THE LAST VALUE IS OUTSIDE THE ROD..... | 148 |
| FIGURE 4-10 CROSS SECTION OF A FERRITE BOBBIN CORE WITH WINDING WINDOW..... | 150 |
| FIGURE 4-11 DEPENDENCE OF MUTUAL ENERGY ON DOMAIN SIZE. E_B = CONSTANT FIELD ENERGY, E_{I_2} = PICKUP CURRENT ENERGY, E_M = MUTUAL FIELD ENERGY, E_T = TOTAL DOMAIN FIELD ENERGY AND Φ_2 = MAGNETOMETRIC FLUX. | 151 |
| FIGURE 4-12 M_{core} AS A FUNCTION LENGTH/DIAMETER WITH DIFFERENT CURVES FOR μ_r VALUES RANGING FROM 10 -10000. | 152 |
| FIGURE 4-13 LENGTH IS REQUIRED IN ORDER FOR A FERRITE TO DRAW IN FLUX FROM THE SURROUNDING REGION THROUGH LOWER RELUCTIVITY | 153 |
| FIGURE 4-14 ERROR BETWEEN ANSYS GENERATED μ_{core} AND DEMAGNETISATION FACTORS FROM CHEN ET AL FOR μ_r OF 10, 100 AND 1000. | 155 |
| FIGURE 4-15 EFFECTIVE PICKUP AREA AS A FUNCTION PERMEABILITY WITH ORIGINAL DATA REPRESENTED BY CROSSES AND THE MODEL AS SOLID LINES. | 156 |
| FIGURE 4-16 COMPONENTS OF THE ENERGY IN THE FINITE ELEMENT MODEL AS A FUNCTION OF THE WINDING HEIGHT AND WIDTH, WHICH ARE GIVEN AS A PERCENTAGE OF THE FERRITE HEIGHT AND RADIUS RESPECTIVELY | 158 |
| FIGURE 4-17 COMPARISON OF THE FLUXMETRIC AND MAGNETOMETRIC μ_{core} OF A PICKUP. FLUXMETRIC (ABOVE LEFT) AND MAGNETOMETRIC (ABOVE) μ_{core} AS A FUNCTION OF WINDING SIZE WITH A 1:1 LENGTH TO DIAMETER RATIO BOBBIN CORE. PLOT OF MAGNETOMETRIC DIVIDED BY FLUXMETRIC A_E (LEFT) REVEALS THE DIFFERENCE BETWEEN THE TECHNIQUES. THE COMPARISON PLOTS THE ESTIMATES SQUARED, AS THIS IS PROPORTIONAL TO THEIR PREDICTION OF POWER DELIVERED. THIS PLOT HAS ITS X AND Y AXES REVERSED FOR CLARITY. | 159 |
| FIGURE 4-18 A COMPARISON OF ENERGY AND FLUX BASED μ_{core} FOR DIFFERENT ASPECT RATIOS (HEIGHT:DIAMETER) CORES.. | 161 |
| FIGURE 5-1 SCHEMATIC DIAGRAM OF THE PROTOTYPE LINK. DASHED LINES REPRESENT ISOLATION BETWEEN THE TELEMETER AND PRIMARY. | 168 |
| FIGURE 5-2 PROTOTYPE INDUCTIVE LINK WITH 6 COIL PCB WINDING AND RESONANT INVERTER. LEFT: RESONANT INVERTER. CENTRE FRONT: SPI TO PARALLEL CONVERTER FOR DRIVING SWITCHES. RIGHT: NORDIC DEVELOPMENT KIT WHICH ACTS | |

| | |
|--|-----|
| AS THE CONTROLLER. CENTRE REAR: PROTOTYPE PRIMARY WINDING UNDER WHICH THE COIL SELECTION SWITCHES ARE HIDDEN. | 169 |
| FIGURE 5-3 FLOW DIAGRAM FOR THE DESIGN OF THE INDUCTIVE LINK..... | 171 |
| FIGURE 5-4 MODELLED RESISTANCE OF THE PRIMARY WINDING INCLUDING EDDY CURRENT LOSSES AND SPACES BETWEEN TRACKS | 173 |
| FIGURE 5-5 PREDICTED POWER TRANSFER FROM 6 COIL RECTANGULAR PCB WINDING AT A HEIGHT OF 3CM ABOVE THE PCB..... | 174 |
| FIGURE 5-6 POWER CONDITIONING CIRCUITRY FOR THE TELEMETER. L_2 AND C_2 ARE THE PICKUP COIL AND TUNING CAPACITOR. A 5MA CURRENT SOURCE IS USED TO CHARGE A 680MF TANTALUM BACKUP STORAGE CAPACITOR WHEN POWER IS AVAILABLE. WHEN POWER IS LOST, D3 CONDUCTS MAINTAINING THE INPUT SUPPLY TO THE VOLTAGE REGULATOR..... | 176 |
| FIGURE 5-7 LAYOUT OF THE MOUSE TELEMETER SHOWING TWO PCBs WHICH HOLD TELEMETRY AND POWER CONDITIONING CIRCUITRY..... | 177 |
| FIGURE 5-8 EXPERIMENTAL PICKUP COIL WITH TELEMETRY CIRCUIT AND POWER BOARD INSIDE. VISIBLE IS THE BLUE 2.4GHZ ANTENNA. | 178 |
| FIGURE 5-9 SINGLE CAPACITOR AND MULTI-CAPACITOR IMPLEMENTATIONS OF THE LINK FOR PARALLEL AND SERIES RESONANT OPERATION | 180 |
| FIGURE 5-10 JIG WHICH ALLOWS POSITIONING WITHIN FOUR DEGREES OF FREEDOM. THE SECONDARY COIL IS IN THE CENTRE OF THE CIRCULAR COMPONENT (RUSSELL ET AL., 2009)..... | 181 |
| FIGURE 5-11 BLOCK DIAGRAM OF MEASUREMENT SYSTEM | 182 |
| FIGURE 5-12 COMPARISON OF THE PREDICTED AND MEASURED POWER TRANSFER IN MW: (A) PREDICTED POWER TRANSFERRED WITH COVERAGE AREA INSIDE WHITE BOX. (B) EXPERIMENTALLY MEASURED POWER. | 184 |
| FIGURE 5-13 TRANSIENT PERFORMANCE OF THE INDUCTIVE LINK. (A) START UP AND SHUT DOWN OF THE PRIMARY: EXPERIMENTALLY MEASURED RESONANT CURRENT (BLUE) AND ENVELOPE MODEL AS GIVEN BY EQUATION 2–60 (BLACK). (B) EXPERIMENTALLY MEASURED RESPONSE OF THE PICK UP WHEN LOADED RESISTIVELY (RED) AND ENVELOPE MODEL AS GIVEN BY EQUATION 2–69 (BLACK)..... | 185 |
| FIGURE 5-14 (A) START UP OF THE POWER RECEIVER CIRCUITRY IN FIGURE 5-6. RESONANT INVERTER OUTPUT CURRENT (BLUE) AND V_{BULK} (BLACK). AT $T = 0$ A NEW COIL IS TRIED RESULTING IN C3 IN FIGURE 5-6 CHARGING WITH A TIME CONSTANT OF $700\mu s$. (B) STORAGE CAPACITOR VOLTAGE (BLACK) DURING A 10MS POWER ABSENCE..... | 186 |
| FIGURE 5-15 WAVEFORMS DEMONSTRATING THE SYSTEM’S ABILITY TO CONTINUOUSLY POWER A TELEMETER. CH1 –CH6: AC SWITCH CONTROL LINES. V_{RECT} : VOLTAGE AFTER THE RECTIFIER. V_{BUS} : THE TELEMETER SUPPLY BUS WHICH DRAWS POWER FROM THE PICKUP OR BACKUP CAPACITOR WHEN POWER IS UNAVAILABLE. POWER GOOD: DIGITAL LINE INDICATING THAT THE TELEMETER AND SUBSEQUENTLY THE POWER CONTROLLER HAVE DETECTED THAT SUFFICIENT POWER IS AVAILABLE. | 188 |
| FIGURE 6-1 CROSS SECTIONAL VIEW OF PRESSURE CHAMBER. THE RIG FEATURES A RESERVOIR ON TOP WHICH ALLOWS FITTINGS TO BE ATTACHED UNDER A BATH OF FLUID – REDUCING THE CHANCES OF TRAPPING AIR IN THE PRESSURE CHAMBER.... | 197 |
| FIGURE 6-2 SCHEMATIC DIAGRAM OF FREQUENCY RESPONSE TEST SYSTEM. USING A REFERENCE TRANSDUCER OF KNOWN OR HIGHER BANDWIDTH THAN THE DUT ENSURES THAT THE RESULTS REFLECT THE TELEMETERS PROPERTIES AND NOT ARTEFACTS OF THE FLUID CHAMBER. | 198 |

| | |
|---|-----|
| FIGURE 6-3 TRANSFER FUNCTION FROM CONTROL TO VOICE COIL CURRENT. NEGATIVE FEEDBACK AROUND THE VOICE COIL CURRENT RESULTS IN A FLAT RESPONSE WITHIN 3DB TO APPROXIMATELY 8 KHZ | 199 |
| FIGURE 6-4 MAGNITUDE RESPONSE OF THE PRESSURE GENERATOR WITH DIFFERENT BRASS MEMBRANES: 100 μM BRASS (DASHED LINE), 100 μM BRASS WITH ITS 'BACK BROKEN' (DASH-DOT), HYDROSTATICALLY FORMED 50μM BRASS (DOTTED LINE) AND HYDROSTATICALLY FORMED 100μM BRASS (SOLID). | 200 |
| FIGURE 6-5 HYDROSTATIC MOULDING OF THE TRANSDUCER SHIM. A SHEET OF BRASS IS COMPRESSED BETWEEN A URETHANE RUBBER AND FORMING DIE. APPLYING PRESSURE DEFORMS THE URETHANE; FORMING THE BRASS TO THE SHAPE OF THE DIE WITHOUT TEARING THE SHIM AS CAN OCCUR WITH A CONVENTIONAL MALE AND FEMALE MOULD. | 201 |
| FIGURE 6-6 AVERAGE FREQUENCY RESPONSE OF DSI'S PA-C10 (N = 4), PA-C40 (N = 4) AND PA-D70 (N = 4), AND TR'S TR43P (N=4) TELEMETERS WITH RAW DATA FROM INDIVIDUAL TELEMETERS IN GREY. | 202 |
| FIGURE 6-7 A COMPARISON REVEALS THAT FREQUENCY RESPONSE IS ONLY SLIGHTLY INVERSELY PROPORTIONAL TO DEVICES' SIZE OR CATHETER DIMENSION. | 203 |
| FIGURE 6-8 COMPARISON OF THE -3DB RESPONSES OF INDIVIDUAL TELEMETERS WHEN SORTED BY DEVICE TYPE. | 205 |
| FIGURE 6-9 DIMENSIONS OF THE CATHETERS UNDER TEST. THE CATHETERS' FREQUENCY RESPONSE WERE TESTED AS THE AMOUNT OF GEL X WAS INCREASED. | 206 |
| FIGURE 6-10 TRANSFER FUNCTION FROM CATHETER TIP TO PRESSURE SENSOR OUTPUT AS GEL IS ADDED TO THE DISTAL TIP. THE RECORDINGS CLEARLY SHOW THE DAMPENING EFFECT OF ADDING GEL TO THE DISTAL TIP. 0 MM MEANS THAT NO GEL WAS USED AND THE TIP IS FILLED WITH PRESSURE TRANSMISSION FLUID. 1 MM MEANS THAT 1 MM OF GEL WAS APPLIED WITH THE REMAINDER FILLED WITH FLUID. | 207 |
| FIGURE 6-11 -3DB FREQUENCY VERSUS QUANTITY OF GEL WITH SEM FOR N = 4 CATHETERS. INITIALLY THE GEL HAS LITTLE EFFECT ON BANDWIDTH BUT ROLLS OFF STEADILY AFTER THE TIP IS HALF FULL. THE -3DB FREQUENCY IS STILL ADEQUATE FOR MEASUREMENTS WITH UP TO 6 MM OF GEL. | 208 |
| FIGURE 6-12 FREQUENCY RESPONSE FOR ONE TR43P PLOTTED AS A FUNCTION OF HOW MUCH OF ITS TIP HAS BEEN REMOVED. CUTTING THE TIP OFF HAS VERY LITTLE EFFECT ON THE FREQUENCY RESPONSE UNTIL THE ENTIRE THIN WALLED PORTION OF THE CATHETER HAS BEEN REMOVED (7 MM). | 210 |
| FIGURE 6-13 A COMPARISON OF THE MEASURED AND FITTED TRANSFER FUNCTIONS FOR THE TR43P AND PA-C40 SHOWING MAGNITUDE RESPONSE (UPPER TRACE) AND PHASE RESPONSE (LOWER TRACE). TRANSFER FUNCTIONS WERE FITTED WITH AN EMPHASIS ON THE LOWER FREQUENCIES WHICH ARE MOST IMPORTANT FOR ACCURATE SIMULATIONS. SIMULATED AND MEASURED RESPONSES BEGIN TO DIVERGE AT HIGHER FREQUENCIES WHERE THE ATTENUATION IS LARGE. | 213 |
| FIGURE 6-14 HIGH FIDELITY ORIGINAL SIGNAL (BLACK LINE) PASSED THROUGH MODEL OF PA-C40 (BLUE) FILTER RESPONSE AND MODEL OF TR43P (RED) FILTER RESPONSE. THESE ARE THE ORIGINAL OUTPUTS FROM SIMULATION INCLUDING TRANSMISSION DELAY. | 214 |
| FIGURE 6-15 BOTTOM: CLOSE UP OF ALIGNED WAVEFORMS DEMONSTRATING BOTH DEVICES CAPTURE THE WAVEFORM WITH GOOD FIDELITY. COLOURING IS THE SAME AS FIGURE 6-14. | 215 |
| FIGURE B-1 SOLID-STATE AC SWITCH DESIGN FOR PRIMARY COIL CONTROL..... | 241 |
| FIGURE B--2 DEAD TIME CIRCUIT OUTPUT (MOCD207) CURRENT AS A FUNCTION CONTROL LINE VOLTAGE. | 242 |

LIST OF TABLES

| | |
|---|-----|
| TABLE 1-1. A COMPARISON OF THE FEATURES OF WIRELESS POWER TRANSFER ENABLED TELEMETER VERSUS A BATTERY OPERATED DEVICE. | 6 |
| TABLE 2-1 PRIMARY PROPERTIES | 48 |
| TABLE 2-2 PICKUP PROPERTIES | 49 |
| TABLE 2-3 PREDICTED POWER TRANSFERRED TO THE LOAD | 50 |
| TABLE 2-4 USEFUL RELATIONSHIPS FOR LOOSELY COUPLED LINKS (ADAPTED FROM LENAERTS AND PUERS (LENAERTS AND PUERS, 2008)). EQUATIONS IN BOLD TYPE ARE CONTRIBUTIONS OF THIS THESIS WHICH HAVE BEEN ADDED TO THE TABLE. | 70 |
| TABLE 5-1 POWER REQUIREMENTS OF THE TELEMETER..... | 167 |
| TABLE 5-2. PROPERTIES OF THE PROTOTYPE INDUCTIVE LINK..... | 175 |
| TABLE 6-1 AVERAGE FREQUENCY RESPONSES OF TELEMTRY DEVICE AND RESULTS OF NON PARAMETRIC ANALYSIS | 205 |

NOMENCLATURE AND SYMBOLS

Acronyms

| | | |
|--------|---|---|
| 2D | - | Two Dimensions |
| 3D | - | Three Dimensions |
| AC | - | Alternating Current |
| ADC | - | Analogue to Digital Converter |
| AWG | - | American Wire Gauge |
| BP | - | Blood Pressure |
| BPM | - | Beats Per Minute |
| DC | - | Direct Current |
| DUT | - | Device Under Test |
| EMI | - | Electromagnetic Interference |
| ESR | - | Equivalent Series Resistance |
| HF | - | High Frequency |
| ICPT | - | Inductively Coupled Power Transfer |
| ISM | - | Industrial Scientific and Medical (Band) |
| LC | - | Inductor-Capacitor connection |
| LR | - | Inductor-Resistor connection |
| MOSFET | - | Metal Oxide Semiconductor Field Effect Transistor |
| OD | - | Outside Diameter |
| PCB | - | Printed Circuit Board |
| PWM | - | Pulse Width Modulation |
| QFN | - | Quad Flat No leads |
| RF | - | Radio Frequency |
| RMS | - | Root Mean Square |
| SEM | - | Standard Error of the Mean |
| SNA | - | Sympathetic Nerve Activity |
| SOC | - | System On Chip |
| SPI | - | Serial Peripheral Interface |
| TET | - | Transcutaneous Energy Transfer |

Symbols

Fundamental Quantities

| | | |
|-----------------------------------|---|----------------------------------|
| $\vec{a}_x, \vec{a}_y, \vec{a}_z$ | - | Cartesian Unit Vector |
| B | - | Magnetic Field Magnitude (Tesla) |
| \mathbf{B} | - | Magnetic Field Vector (Tesla) |
| C | - | Capacitor (Farads) |
| δ | - | Skin Depth (m) |
| E | - | Energy (Joules) |
| f | - | Frequency (Hz) |
| $G(s/j\omega)$ | - | Transfer Function |

| | | |
|--------------|---|---|
| i | - | Instantaneous Current / Envelope of Current (Amperes) |
| I | - | Current Magnitude (Amperes) |
| j | - | Complex Operator ($\sqrt{-1}$) |
| k | - | Magnetic Coupling Coefficient |
| L | - | Self-Inductance (Henrys) |
| λ | - | Flux Linkages (Volt Second/Weber Turns) |
| M | - | Mutual Inductance (Henrys) |
| μ | - | Permeability (H/m) |
| μ_0 | - | Vacuum Permeability (H/m) |
| μ_r | - | Relative Permeability (Unit-less) |
| \mathbf{n} | - | Unit Normal Vector |
| Φ | - | Magnetic Flux (Weber) |
| ω | - | Angular Frequency (Radians/s) |
| Q | - | Quality Factor |
| r | - | Radius (m) |
| R | - | Resistance (Ω) |
| ρ | - | Resistivity ($S \cdot m^{-1}$) |
| t | - | Time (seconds) |
| T | - | Period (seconds) |
| τ | - | Time Constant (seconds) |
| θ | - | Phase Angle |
| v | - | Instantaneous Voltage (Volts) |
| V | - | Voltage Magnitude (Volts RMS) |
| V_{FW} | - | Diode Forward Voltage (Volts) |
| W | - | Power (Watts) |

Primary Symbols

| | | |
|-----------------|---|---|
| a, b | - | Outside Dimensions of Rectangular Coil (m) |
| B_0 | - | Normalized Magnetic Field Strength ($B/(N_1 I_1)$) |
| B_{0-min} | - | Global or Local Minimum Field Strength ($B/(N_1 I_1)$) |
| C_1 | - | Primary Tuning Capacitance (Farads) |
| d_i | - | Spiral Coil Inner Diameter (m) |
| d_o | - | Spiral Coil Outer Diameter (m) |
| E_{LI} | - | Primary Winding Energy (Joules) |
| I_1 | - | Primary Current (A_{RMS}) |
| L_{10} | - | Single Turn Equivalent Primary Self-inductance (Henrys) |
| L_1 | - | Primary Self-inductance (Henrys) |
| l_c | - | Conductor Length (m) |
| N_1 | - | Primary Turns |
| W_h | - | Window Height (m) |
| ω_{crit} | - | Frequency Where 10% of R is Due to Eddy Current (rads/s) |
| R_1 | - | Primary Winding Resistance (Ω) |

| | | |
|----------|---|--|
| R_{10} | - | Single Turn Equivalent Primary Winding Resistance (Ω) |
| s | - | Space between Adjacent Tracks (m) |
| t_c | - | Sheet Conductor Thickness (m) |
| w | - | Track Width (m) |
| X_1 | - | Primary Winding Potential (Vs^2/Am^4) |

Secondary (Pickup) Symbols

| | | |
|--------------|---|--|
| A_c | - | Pickup Area (m^2) |
| A_e | - | Effective Pickup Area (m^2) |
| η_2 | - | Secondary Efficiency |
| β | - | $N_2/N_{2\text{ PMAX}}$ |
| C_2 | - | Secondary Tuning Capacitance (Farads) |
| E_{L2} | - | Secondary Winding Energy (Joules) |
| F | - | Fill Factor (Unit-less) |
| I_2 | - | Secondary Current (A_{RMS}) |
| I_{sc} | - | Short Circuit Current (A_{RMS}) |
| L_2 | - | Secondary Self-inductance (Henrys) |
| L_{20} | - | Single Turn Equivalent Secondary Self-inductance (Henrys) |
| N_2 | - | Secondary Turns |
| N_f | - | Fluxmetric Demagnetizing Factor |
| N_m | - | Magnetometric Demagnetizing Factor |
| Q_2 | - | Secondary Quality factor |
| R_2 | - | Secondary Winding Resistance (Ω) |
| R_{20} | - | Single Turn Equivalent Secondary Winding Resistance (Ω) |
| R_L | - | Load Resistance (Ω) |
| R_{L0} | - | Single Turn Equivalent Secondary Load (Ω) |
| Γ | - | Ratio of Length upon Diameter |
| V_{OC} | - | Open Circuit Voltage (V_{RMS}) |
| W_h | - | Window Height (m) |
| W_r | - | Window Radius (m) |
| X_2 | - | Secondary Winding Potential (Am^4/ V) |
| μ_{core} | - | Effective Core Permeability $\equiv A_e/A_c$ (unit-less) |

Link Properties

| | | |
|--------|---|----------------------------------|
| A | - | Link Gain (Unit-less) |
| η | - | Efficiency (Unit-less) |
| E_M | - | Mutual Energy (Joules) |
| k | - | Coupling Coefficient (Unit-less) |

| | | |
|------------|---|---|
| M | - | Mutual inductance (Henrys) |
| M_0 | - | Single Turn Equivalent Mutual inductance (Henrys) |
| P_{IN} | - | Input Power (Watts) |
| P_{OUT} | - | Output Power (Watts) |
| ω_0 | - | Resonant Frequency (Radians) |
| X | - | Link Potential (Unit-less) |

Subscripts

| | | |
|------------|---|---|
| 1 | - | Primary Component |
| 2 | - | Secondary Component |
| 10 | - | Single Turn Equivalent Primary Component |
| 20 | - | Single Turn Equivalent Secondary Component |
| AC | - | AC value |
| $const$ | - | Constant Quantity |
| DC | - | DC value |
| ΔV | - | Quantity Evaluated over a Partial Volume |
| eq | - | Equivalent |
| E | - | Eddy Component (of Resistance) |
| MAX | - | Maximum value or value at which maximum is obtained |
| MIN | - | Minimum value |
| OC | - | Open circuit |
| P | - | Peak |
| $Pk-Pk$ | - | Peak to Peak |
| PAR | - | Parallel Equivalent |
| REF | - | Reference |
| RMS | - | Root Mean Square |
| SER | - | Series Equivalent |
| SC | - | Short circuit |
| x,y,z | - | Cartesian Component of Quantity |